

Rise in Core Wettability Characterization Technique

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Outline

- Background
- Objectives
- Theoretical Approach
- Experimental Setup and Procedure
- Results and Discussion
- Comparison with Industry Standard Method
- Conclusions & Recommendations
- Acknowledgements



Wettability

- Wettability is defined as the relative preference of a solid surface to be coated by a certain fluid in a system.
- The reservoir rock wetting preference influences many aspects of reservoir performance:
 - Controls the fluid flow directly,
 - Affect the location and distribution of fluids,
 - Affect Oil Trapping Mechanism.

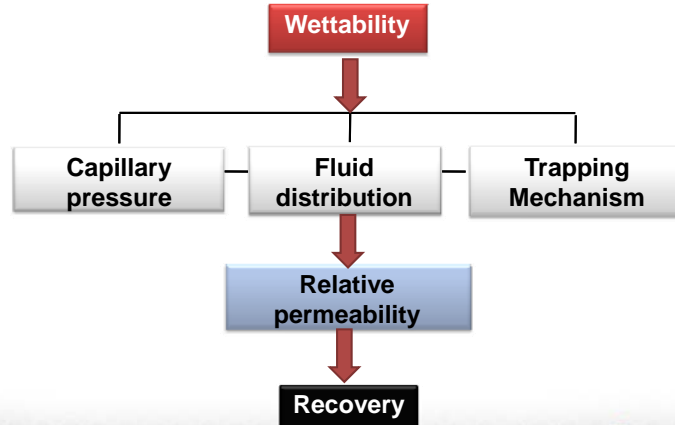


Range and Alteration of Wettability

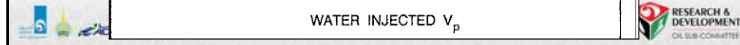
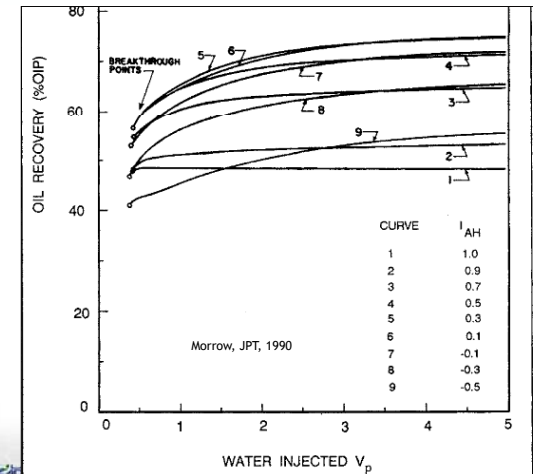
- Reservoir wettability is affected by the:
 - Minerals in the pores as well as their distribution.
 - Adsorption or deposition of oil constituents on the rock surface.
 - The oil composition, as black-oil composition determines the solubility of the polar components.
 - Reservoir Conditions of temperature, pressure and saturation history.



Why Wettability is Important



Performance of Waterflooding

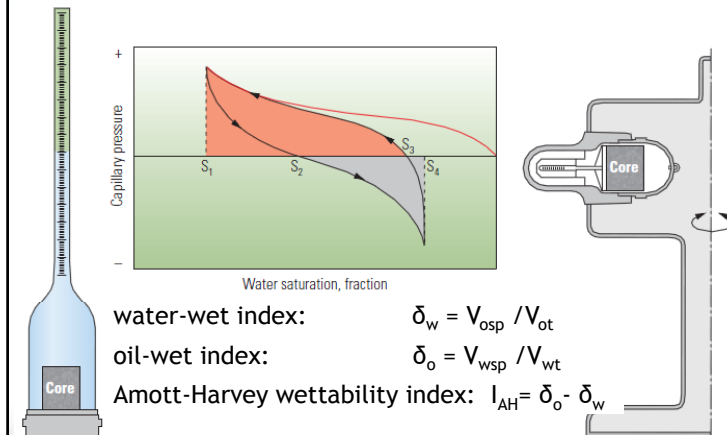


Measurement Techniques

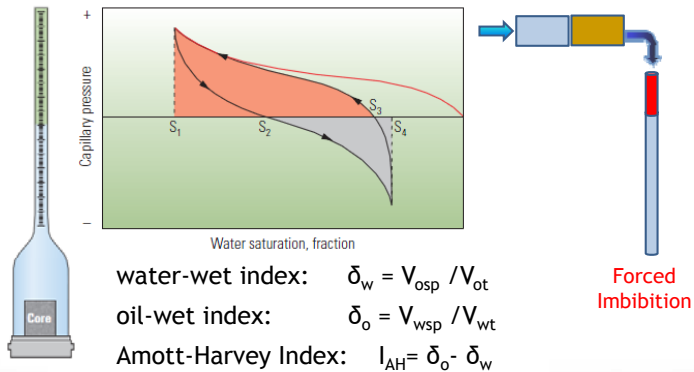
- Industrial wettability measuring techniques include:
 - Amott Wettability Methods,
 - USBM Wettability Method,
 - Combined Amott-Harvey & USBM Methods, and
 - Contact Angle Methods.
- Limitations:
 - Imprecise in Wettability bands.
 - Very Demanding Experimental Setup.
 - Very Demanding Experimental Procedure
 - USBM test cannot determine whether a system has fractional or mixed wettability.



Amott-Harvey Method



Amott-Harvey Method

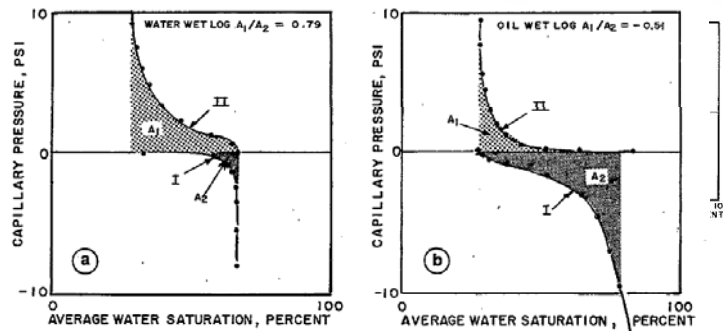


Advantages and Disadvantages

- Advantage:
 - Relatively quick method (days).
- Disadvantages:
 - Insensitive near neutral wettability.
 - Measures Wettability by an Index



USBM Wettability Index



$W = \log(A_1 / A_2)$ A_1 and A_2 are the areas under the oil- and brine-drive curves respectively.

If $W > 0$, water-wet; $W < 0$, oil-wet; $W \approx 0$, neutrally wet.

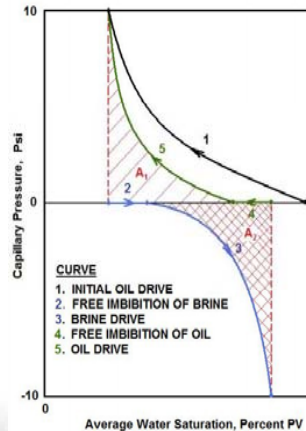


Advantages and Disadvantages

- Advantage:
 - USBM is more sensitive to near neutral wettability.
- Disadvantages:
 - Time Consuming
 - USBM WI = $-\infty$ to ∞
 - Insensitive to fractional or mixed wettability.
 - Expensive



Modified Amott - USBM Method



Procedure of five steps :
 (1) Initial Oil Drive,
 (2) Brine Spontaneous Imbibition,
 (3) Brine Drive,
 (4) Oil Spontaneous Imbibition
 (5) Oil Drive.

USBM WI: The areas under the brine-and oil-drive curves.

While,
 Amott WI: Volumes of free and total water and oil displacements.



Call for New Technique

- Drawbacks of existing techniques call for the inventing a new technique to characterize wettability that has the following attributes:
 - (a) Sound Theoretical Background
 - (b) Simpler experimental setup,
 - (c) Conducted with less experimental effort,
 - (d) Determine all bands of wettability,
 - (e) if Possible, measure contact angle rather than a wettability index.



RIC Technique

- New Rise In Core Wettability Characterization Technique is proposed.
- Based on a New Liquid/Liquid/rock Washburn equation.
- Estimates Wettability in terms of Contact Angle.
- Proved the RIC Concept Considering Repeatability and Uncertainty using Berea SS Core Samples.
- Compared to Industry standard techniques using Carbonate Core Samples.



Modifying Washburn Equation

- The Washburn equation

$$m^2 = \frac{C \cdot \rho^2 \cdot \gamma_{LV} \cdot \cos\theta}{\mu} \cdot t$$

- Where:

$$C = \left[\frac{r (\pi R_k^2)^2 \phi^2}{2} \right]$$

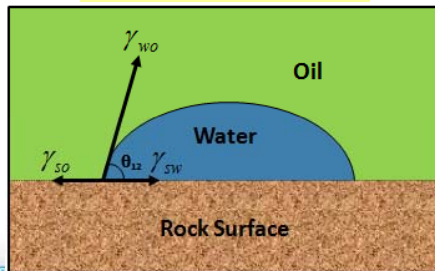
- This version of the Washburn equation enables to describe the contact angles of air/liquid/rock systems. (Wolfrom et al., 2002).



Washburn Eq for Oil/Water System

- Note that Young equation for liquid/liquid/rock systems can be described as (Tiab, 2004),

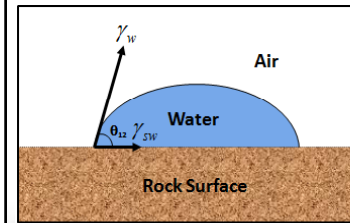
$$\cos \theta_{wo} = \frac{\gamma_{so} - \gamma_{sw}}{\gamma_{wo}}$$



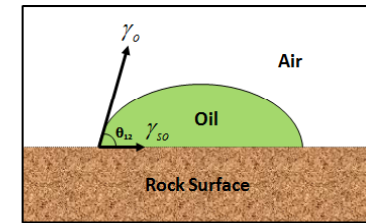
Washburn Eq for Oil/Water System

- Evaluating γ_{sw} and γ_{so} using Figures b and c, and substituting in Equation 3, results in,

$$\cos \theta_{wo} = \frac{(\gamma_{oa} \cos \theta_{oa}) - (\gamma_{wa} \cos \theta_{wa})}{\gamma_{wo}}$$



(b)



(c)



Washburn Eq for Oil/Water System

- Cancelling out similar terms, results in,

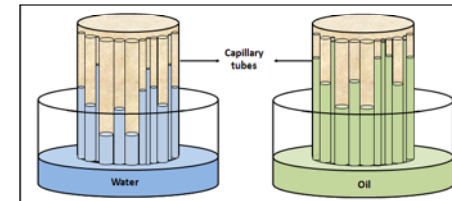
$$\cos \theta_{wo} = \frac{\left(\frac{m^2 \cdot \mu_o}{C \rho_o^2 t} \right) - \left(\frac{m^2 \cdot \mu_w}{C \rho_w^2 t} \right)}{\gamma_{wo}}$$

- Air behaves as strong non-wetting phase in both of oil/air/solid and water/air/solid systems.
- Equal air/oil and air/water capillary forces would result if the differences between $\gamma_{air/oil}$ and $\gamma_{air/water}$ are ignored (assumption).



Washburn Eq for Oil/Water System

- Considering Water/Air and Oil/Air Systems in certain porous media



- For equal capillary forces, both water and oil will rise in pores according to their densities,

$$\rho_w g h_w = \rho_o g h_o$$



Modified W/O Washburn Equation

- Water or oil penetration of the porous media at any time is function of the balance between gravity and capillary forces, resulting in,

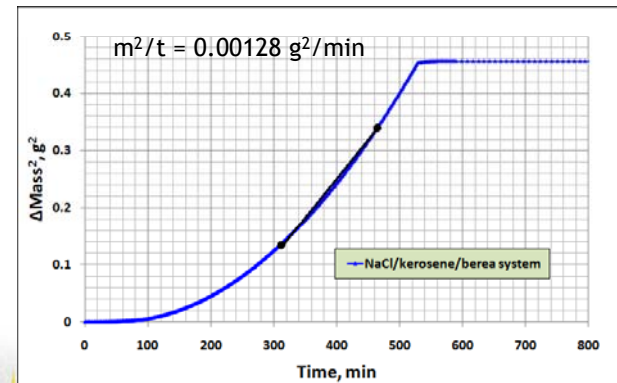
$$\cos \theta_{wo} = \frac{(\mu_o \cdot \rho_w^2) - (\mu_w \cdot \rho_o^2)}{\rho_o^2 \rho_w^2 \cdot C \cdot \gamma_{wo}} \cdot \frac{m^2}{t}$$

- Where,
- The constant, C, characterizes the porous media;
- The term m^2/t could be the slope of the imbibition curves (m^2 vs. time) of both oil/water/solid system.

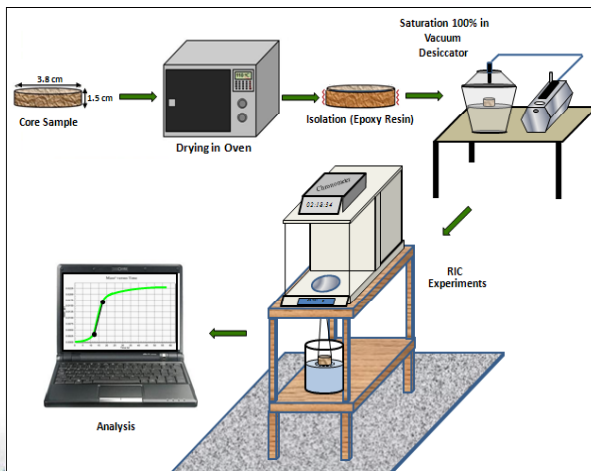


Water/Oil Imbibition Experiment

$$\cos \theta_{wo} = \frac{(\mu_o \cdot \rho_w^2) - (\mu_w \cdot \rho_o^2)}{\rho_o^2 \rho_w^2 \cdot C \cdot \gamma_{wo}} \cdot \frac{m^2}{t}$$



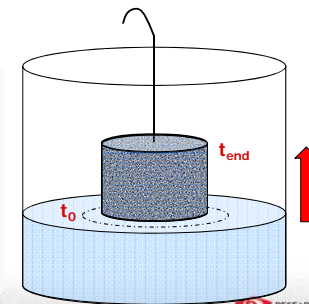
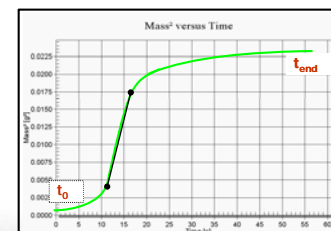
Experimental Setup



RIC Experiments for C Determination

- RIC dodecane/air/rock imbibition experiment performed to determine the m^2/t .

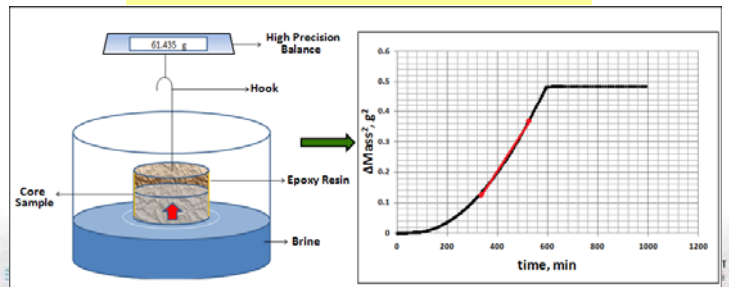
$$C = \frac{\mu}{\gamma_{LV} \cdot \rho^2 \cdot \cos \theta} \cdot \frac{m^2}{t}$$



RIC Experiments for Wettability

- Liquid/Liquid/rock Washburn equation
- RIC is performed with brine/oil system.

$$\cos \theta_{wo} = \frac{(\mu_o \cdot \rho_w^2) - (\mu_w \cdot \rho_o^2)}{\rho_o^2 \rho_w^2 \cdot C \cdot \gamma_{wo}} \cdot \frac{m^2}{t}$$

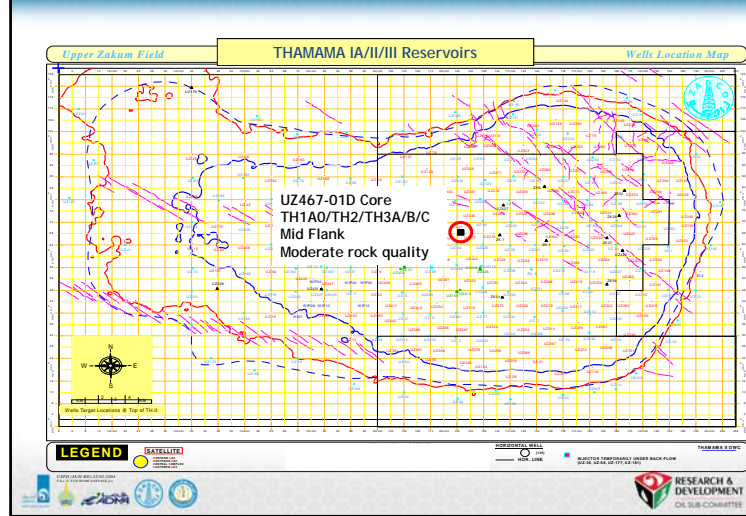


Core Samples

- Cores samples from across the well, but mostly in the crest of the reservoir.
- Core are cut from the proximity of other cores samples to be cut for Amott-Harvey/USBM Wettability Measurements by a third party.



Location of UZ467

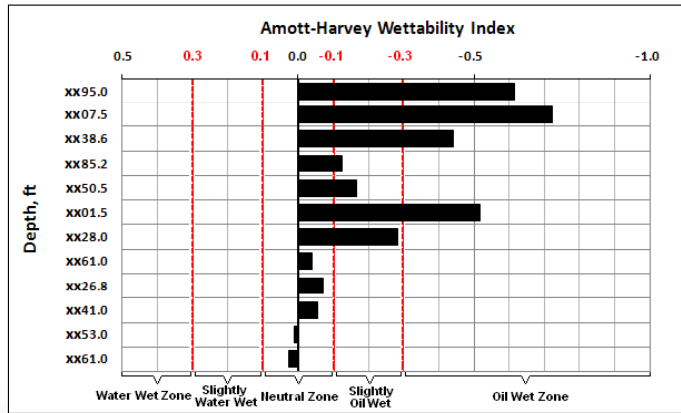


Twin Carbonate Core Samples

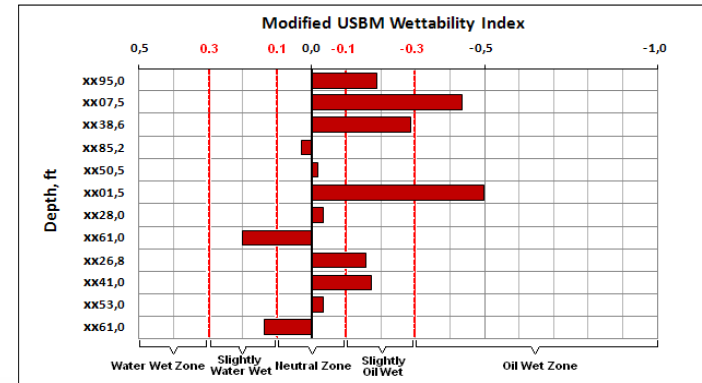
| Formation | Twin Cores | |
|-----------|------------|-----------|
| | Depth, ft | Depth, ft |
| YZ1A | XX95 | XX94.8 |
| YZ1A | XX07.6 | XX07.3 |
| YZ1A | XX38.6 | XX38.4 |
| YZ2 | XX85.2 | XX85.8 |
| YZ2 | XX50.5 | XX50.3 |
| YZ2 | XX01.5 | XX02.0 |
| YZ3A | XX28.0 | XX28.5 |
| YZ3A | XX61.0 | XX61.8 |
| YZ3C | XX26.0 | XX26.6 |
| YZ3C | XX41.0 | XX40.8 |
| YZ3C | XX53.0 | XX52.6 |
| YZ3C | XX61.0 | XX61.4 |



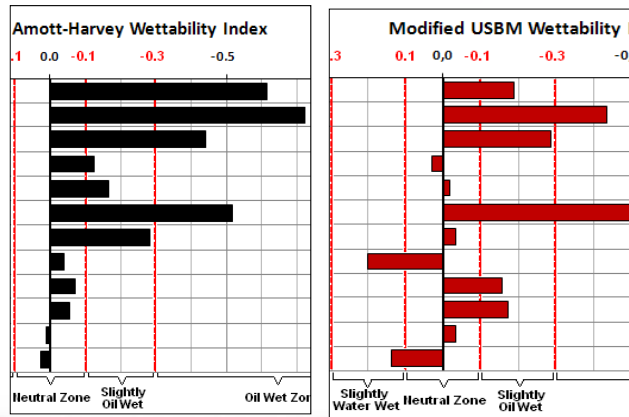
Amott-Harvey Wettability Index



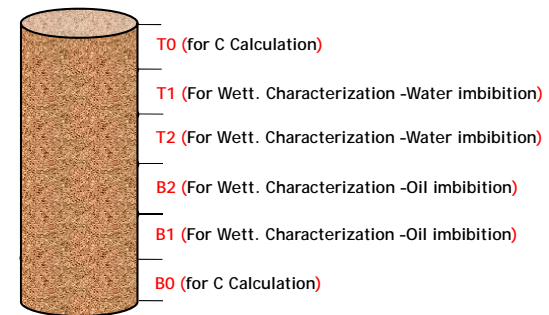
USBM Wettability Index

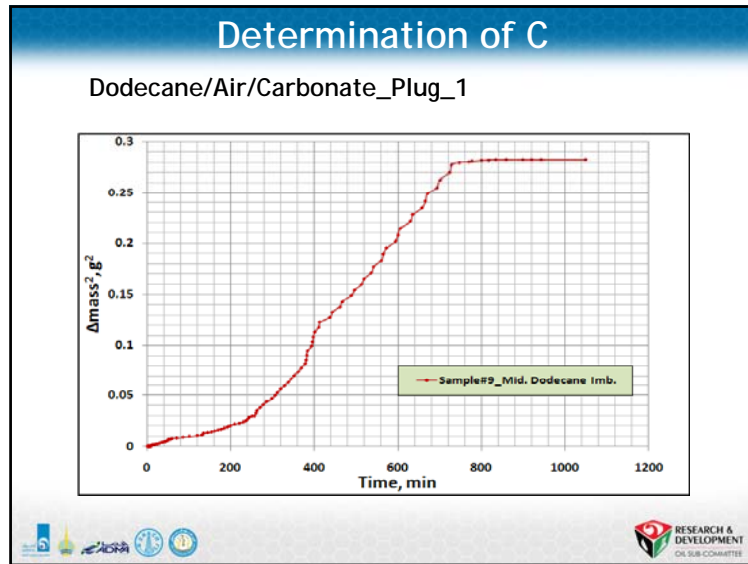


Amott-Harvey vs USBM Wettability Index



RIC Wettability Determination



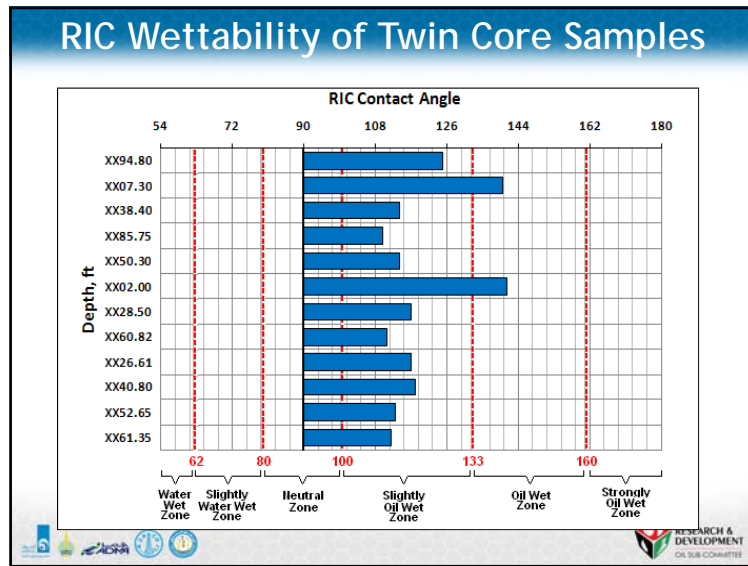


Wettability Measurement

| Top- (Water Imbibition) | | | | Bottom- (Oil Imbibition) | | | |
|-------------------------|--------|--------|---------|--------------------------|--------|--------|---------|
| C Slope | Min | Max | Average | C Slope | Min | Max | Average |
| Min | 119.10 | 115.91 | 117.27 | Min | 117.30 | 114.33 | 115.61 |
| Max | 120.91 | 117.48 | 118.94 | Max | 124.29 | 120.40 | 122.06 |
| Average | 119.73 | 116.45 | 117.85 | Average | 118.92 | 115.75 | 117.11 |

Time, min

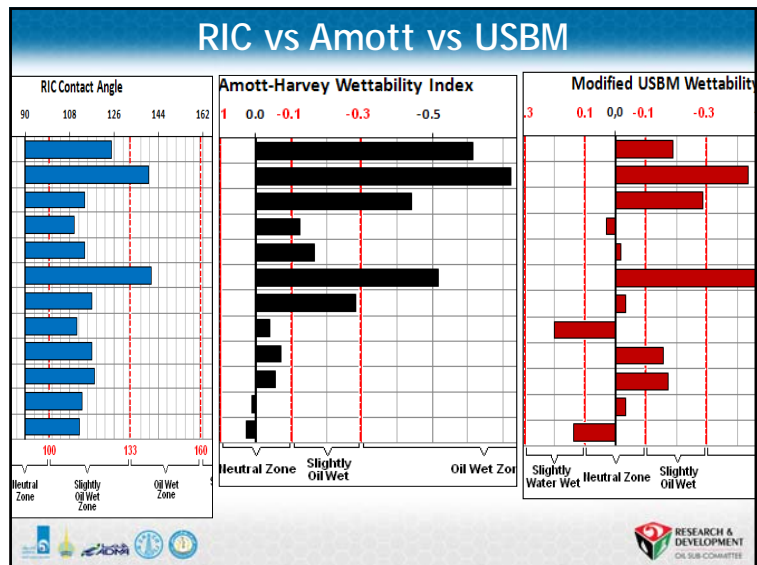
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RIC vs Amott-Harvey and USBM

| Reservoir Formation | Reservoir Depth, ft | Amott-Harvey Index | Wettability Classification | USBM Index | Wettability Classification | Reservoir Depth, ft | RIC Contact Angle | Wettability Classification |
|---------------------|---------------------|--------------------|----------------------------|------------|----------------------------|---------------------|-------------------|----------------------------|
| Y21A0 | XX95.00 | -0.614 | Oil Wet | -0.188 | Slight Oil Wet | XX94.80 | 125 | Slight Oil Wet |
| Y21A0 | XX07.50 | -0.722 | Oil Wet | -0.434 | Oil wet | XX07.30 | 140 | Oil wet |
| Y21A0 | XX38.60 | -0.442 | Mod Oil Wet | -0.285 | Slight Oil Wet | XX38.40 | 114 | Slight Oil Wet |
| Y22 | XX85.20 | -0.124 | Slight Oil Wet | 0.03 | Neutral Wet | XX85.75 | 110 | Slight Oil Wet |
| Y22 | XX50.50 | -0.168 | Slight Oil Wet | -0.017 | Neutral Wet | XX50.30 | 114 | Slight Oil Wet |
| Y22 | XX01.50 | -0.516 | Oil Wet | -0.499 | Oil wet | XX02.00 | 141 | Oil wet |
| Y23A | XX28.00 | -0.282 | Slight Oil Wet | -0.035 | Neutral Wet | XX28.50 | 117 | Slight Oil Wet |
| Y23A | XX61.00 | -0.041 | Neutral Wet | 0.2 | Slight Water Wet | XX60.82 | 111 | Slight Oil Wet |
| Y23C | XX26.80 | -0.071 | Neutral Wet | -0.157 | Slight Oil Wet | XX26.61 | 117 | Slight Oil Wet |
| Y23C | XX41.00 | -0.055 | Neutral Wet | -0.173 | Slight Oil Wet | XX40.80 | 118 | Slight Oil Wet |
| Y23C | XX53.00 | 0.010 | Neutral Wet | -0.033 | Neutral Wet | XX52.65 | 113 | Slight Oil Wet |
| Y23C | XX61.00 | 0.026 | Neutral Wet | 0.138 | Slight Water Wet | XX61.35 | 112 | Slight Oil Wet |

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Way Forward

- Investigate if the Constant, C, (Pore Mean Diameter) could be used to infer rock types.
- Conduct more RIC experiments in Carbonate Cores from Wells drilled in the Transition Zone
- Refine the experimental setup and experimental procedure.
- Extend the Current Experimental Setup and procedure to reservoir conditions.

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